

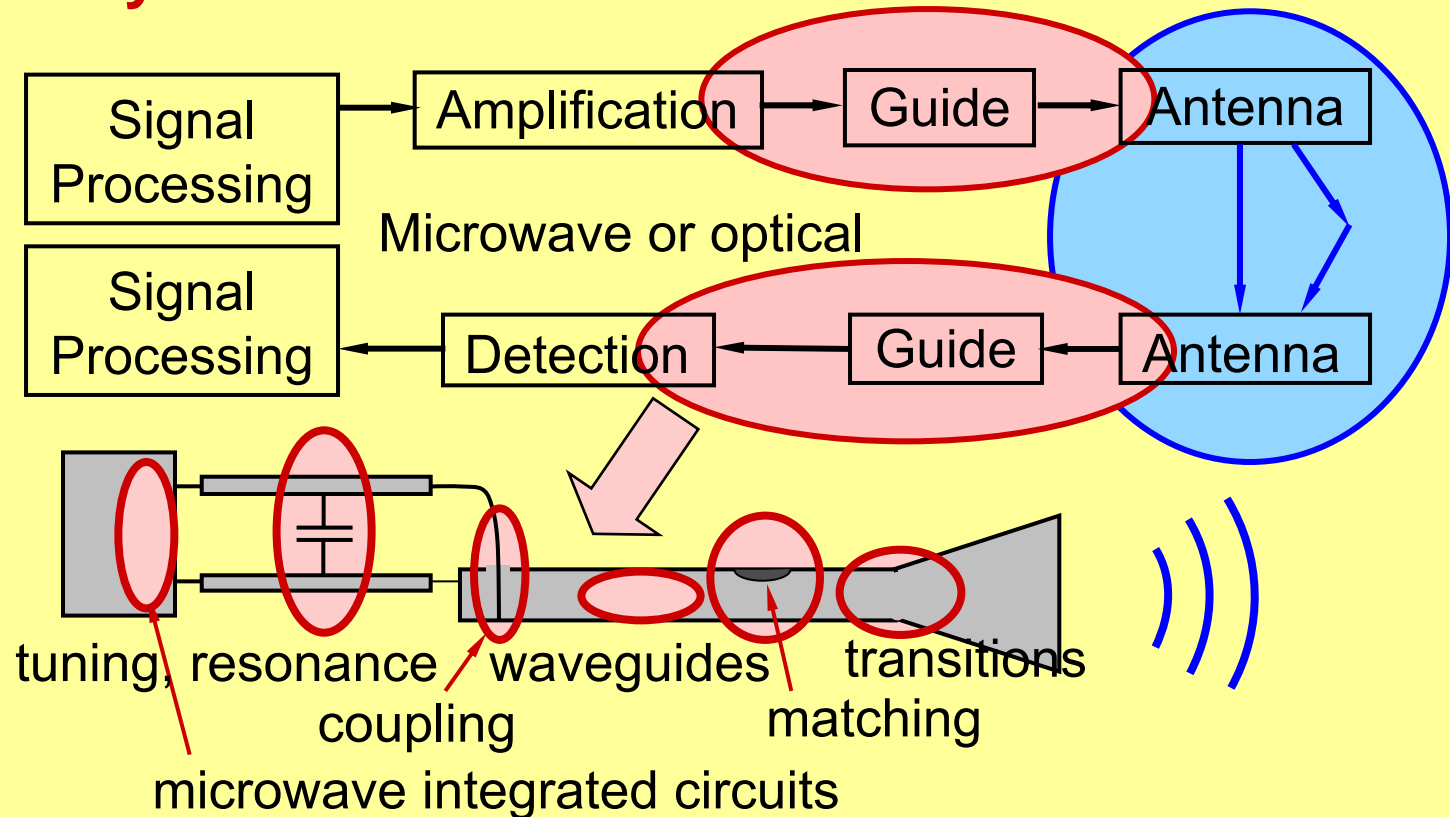
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6.013 Electromagnetics and Applications  
Spring 2009

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# EM GUIDANCE AND FILTERING

## Generic System Architecture:



**Systems fail at weakest link, so understand all parts**

Communications, bi-static radar—separately located systems

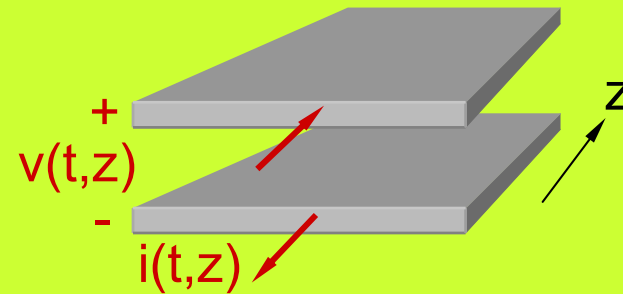
Radar, lidar, data recording—co-located systems

Passive sensing—uses receiver side only

# MICROWAVE CIRCUITS

## Printed Circuits :

$$\text{“TEM”} \Rightarrow \bar{E} \cdot \hat{z} = \bar{H} \cdot \hat{z} = 0$$



## Difference Equations:

$$\underline{V}(z+\Delta z) - \underline{V}(z) = -j\omega L\Delta z \underline{I}(z)$$

$$\underline{I}(z+\Delta z) - \underline{I}(z) = -j\omega C\Delta z \underline{V}(z)$$

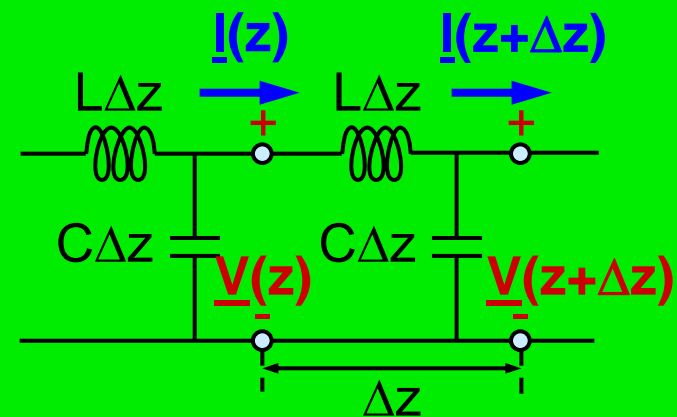
Limit as  $\Delta z \rightarrow 0$ :

$$\frac{d\underline{V}}{dz} = -j\omega L \underline{I}$$

$$\frac{d\underline{I}}{dz} = -j\omega C \underline{V}$$

$$\Rightarrow \frac{d^2\underline{V}(z)}{dz^2} + \omega^2 LC \underline{V}(z) = 0 \quad \text{Wave Equation}$$

## Equivalent TEM line circuit:



# TEM PHASOR EQUATIONS

**Wave Equation:**  $\left(\frac{d^2}{dz^2} + \omega^2 LC\right)\underline{V}(z) = 0$

**Voltage Solution:**  $\underline{V}(z) = \underline{V}_+ e^{-jkz} + \underline{V}_- e^{jkz}$

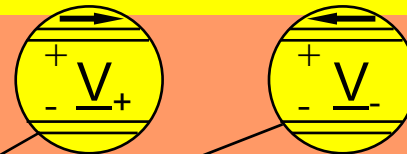
Test solution:  $[(-jk)^2 \underline{V}_+ e^{-jkz} + (jk)^2 \underline{V}_- e^{jkz}] + \omega^2 LC[\underline{V}_+ e^{-jkz} + \underline{V}_- e^{jkz}] = 0$

Passes test iff:  $k^2 = \omega^2 LC$

**Current  $\underline{I}(z)$ :**

Since:  $\frac{\partial \underline{V}(z)}{\partial z} = -j\omega L \underline{I}(z)$

Therefore:  $\underline{I}(z) = \frac{1}{j\omega L} jk(\underline{V}_+ e^{-jkz} - \underline{V}_- e^{+jkz})$   
 $= Y_0(\underline{V}_+ e^{-jkz} - \underline{V}_- e^{+jkz})$



**Line admittance:**

$$Y_0 = \frac{k}{\omega L} = \frac{\omega \sqrt{LC}}{\omega L} = \sqrt{\frac{C}{L}} = \frac{1}{Z_0}$$

**TEM Equations:**

$$\underline{V}(z) = \underline{V}_+ e^{-jkz} + \underline{V}_- e^{jkz}$$

$$\underline{I}(z) = Y_0(\underline{V}_+ e^{-jkz} - \underline{V}_- e^{jkz})$$

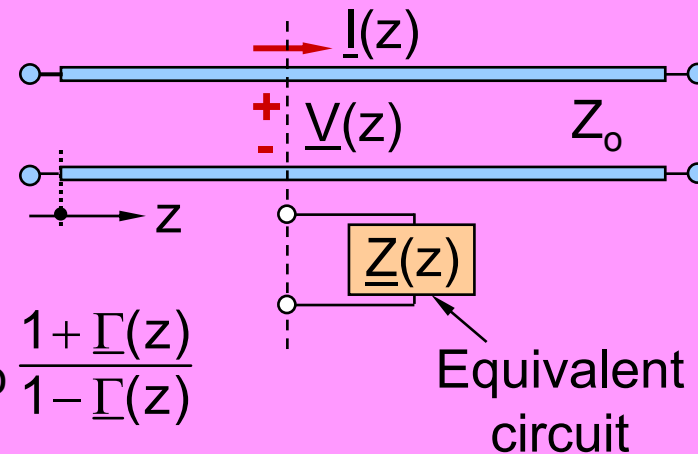
# COMPLEX LINE IMPEDANCE $\underline{Z}(z)$

## Impedance:

$$\underline{Z}(z) = \frac{\underline{V}(z)}{\underline{I}(z)} = R(z) + jX(z)$$

Resistance      Reactance

$$\underline{Z}(z) = \frac{Z_0 (\underline{V}_+ e^{-jkz} + \underline{V}_- e^{jkz})}{\underline{V}_+ e^{-jkz} - \underline{V}_- e^{jkz}} = Z_0 \frac{1 + \underline{\Gamma}(z)}{1 - \underline{\Gamma}(z)}$$



## Complex Reflection Coefficient $\underline{\Gamma}(z)$ :

$$\underline{\Gamma}(z) \triangleq \frac{\underline{V}_- e^{+jkz}}{\underline{V}_+ e^{-jkz}} = \underline{\Gamma}_L e^{2jkz} \quad \text{where } \underline{\Gamma}_L = \underline{\Gamma}(z=0) = \frac{\underline{V}_-}{\underline{V}_+}$$

**Examples:**  $\underline{\Gamma} = 0 \Rightarrow \underline{Z}(z) = Z_0$      $\underline{\Gamma} = 1 \Rightarrow \underline{Z} = \infty$      $\underline{\Gamma} = -1 \Rightarrow \underline{Z} = 0$

## Normalized Impedance $\underline{Z}_n(z)$ :

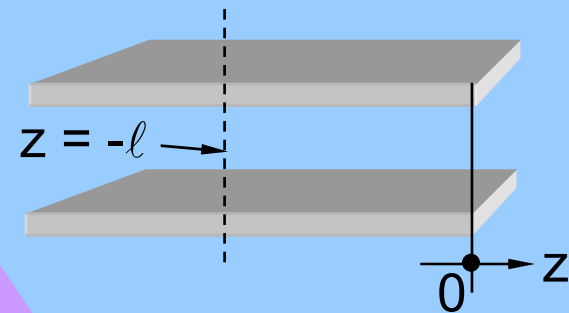
Definition:  $\underline{Z}_n(z) \triangleq \frac{\underline{Z}(z)}{Z_0} = \frac{[1 + \underline{\Gamma}(z)]}{[1 - \underline{\Gamma}(z)]}$  ➔  $\underline{\Gamma}(z) = \frac{[\underline{Z}_n(z) - 1]}{[\underline{Z}_n(z) + 1]}$

# Z(z) TRANSFORMATIONS

Z(z) = f(Z<sub>L</sub>, Z<sub>o</sub>, k, z):

Substituting:  $\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o}$  into  $Z(z) = Z_o \frac{[1 + \Gamma(z)]}{[1 - \Gamma(z)]}$ ;  $\Gamma(z) = \Gamma_L e^{2jkz}$

Yields:  $Z(z) = Z_o \frac{Z_L - jZ_o \tan kz}{Z_o - jZ_L \tan kz}$



**Example: Open Circuit,  $Z_L = \infty$ :**

$$Z(-l) = -jZ_o \cot kl \cong -jZ_o/kl \text{ for } kl \ll 1$$

$$= -j \frac{\sqrt{L/C}}{\omega \sqrt{LC} l} = \frac{1}{j\omega C l}$$

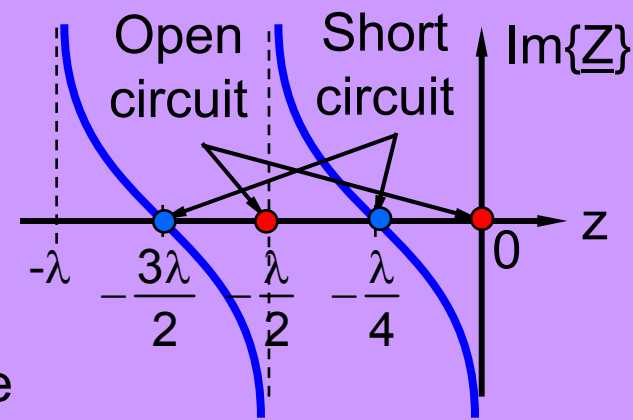
capacitor  $C_o$

$$= 0 \text{ when } z = -\lambda/4, -3\lambda/4, \dots$$

$$= \infty \text{ when } z = 0, -\lambda/2, \dots$$

In general:  $-j\infty < Z(-l) < +j\infty$

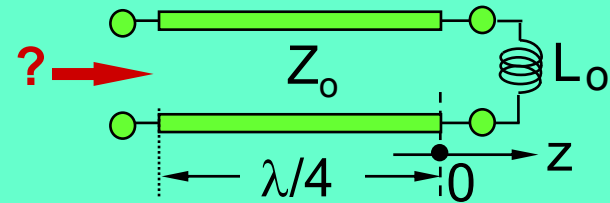
(Yields ANY capacitance or inductance at a SINGLE  $\omega$ )



# EXAMPLES: $\underline{Z}(z)$ TRANSFORMATIONS

## Example—Inductive Load, $\underline{Z}_L = j\omega L_o$ for $z = -\lambda/4$ :

Recall: 
$$\underline{Z}(z) = Z_o \frac{\underline{Z}_L - jZ_o \tan kz}{Z_o - j\underline{Z}_L \tan kz}$$



Since:  $kz = -kl = -\frac{2\pi\lambda}{\lambda} \frac{\lambda}{4} = -\frac{\pi}{2}$ , therefore  $\tan(kz) = -\infty$

Therefore: 
$$\underline{Z}(-l) = \frac{Z_o^2}{\underline{Z}_L} = \frac{L/C}{j\omega L_o} = \frac{1}{j\omega C_o} \quad (C_o = CL_o/L)$$

Note:  $\underline{Z}(z) = j\omega L_o$  if  $l = \lambda/2, \lambda, \dots$  [ $\tan(-2\pi l/\lambda) = 0$ ]

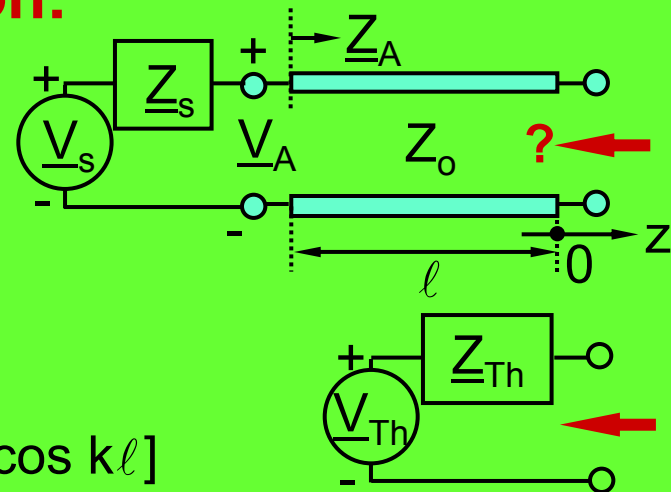
## Example – Source Transformation:

$$\underline{Z}_{Th} = Z_o \frac{\underline{Z}_s + jZ_o \tan kl}{Z_o - j\underline{Z}_s \tan kl}$$

$$\underline{V}_A = \underline{V}_s \frac{\underline{Z}_A}{\underline{Z}_s + \underline{Z}_A} \text{ where } \underline{Z}_A = -jZ_o \cot kl$$

$$= \underline{V}_+ (e^{jkl} + e^{-jkl}) = 2\underline{V}_+ \cos kl$$

Therefore:  $\underline{V}_{Th} = 2\underline{V}_+ = \underline{V}_s \underline{Z}_A / [(\underline{Z}_s + \underline{Z}_A) \cos kl]$



# ALTERNATE APPROACH TO FINDING $\underline{Z}(z)$

Algorithmic, rotate  $\underline{\Gamma}(z)$ :

$$\underline{Z}(z) = \underline{V}(z)/\underline{I}(z) = Z_0 \frac{\underline{V}_+ e^{-jkz} + \underline{V}_- e^{jkz}}{\underline{V}_+ e^{-jkz} - \underline{V}_- e^{jkz}}$$

(1)

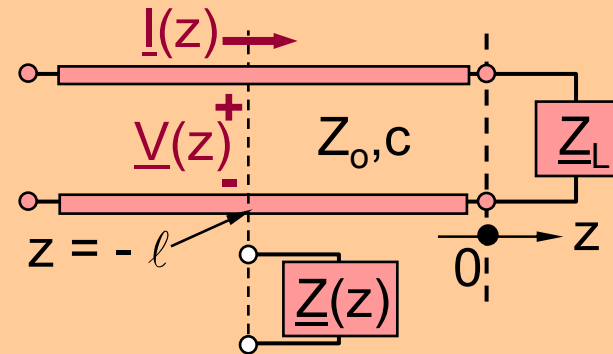
$$\underline{Z}(z) = Z_0 \frac{1 + \underline{\Gamma}(z)}{1 - \underline{\Gamma}(z)}$$

(2)

$$\underline{\Gamma}(z) = \frac{\underline{V}_- e^{+jkz}}{\underline{V}_+ e^{-jkz}} = \underline{\Gamma}_L e^{2jkz} = \underline{\Gamma}(z), \text{ where } \underline{\Gamma}_L = \underline{\Gamma}(z=0) = \frac{\underline{V}_-}{\underline{V}_+}$$

(3)

$$\underline{\Gamma}(z) = \frac{[\underline{Z}_n - 1]}{[\underline{Z}_n + 1]} \quad \underline{Z}_n(z) \triangleq \frac{\underline{Z}(z)}{Z_0}$$



$\underline{\Gamma}$ -Plane Solution Method:

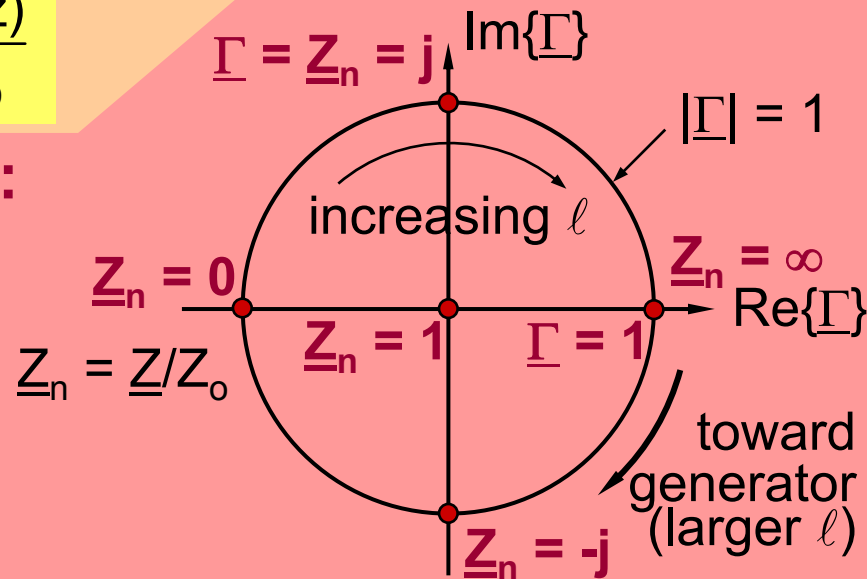
$$\underline{Z}_L \Leftrightarrow \underline{\Gamma}_L \Leftrightarrow \underline{\Gamma}(z) \Leftrightarrow \underline{Z}(z)$$

(3)      (2)      (1)

( $\lambda/2 \Rightarrow$  full rotation)

$e^{-2jkl}$  goes clockwise as  $l \rightarrow \infty$

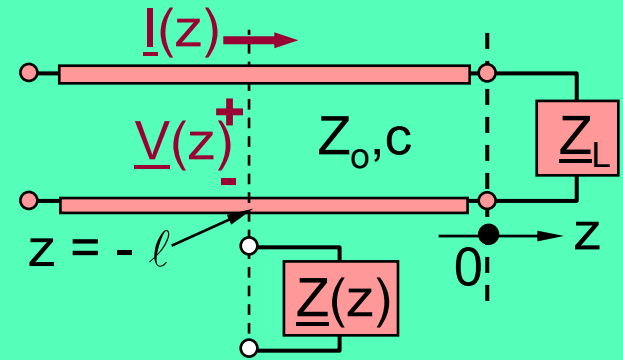
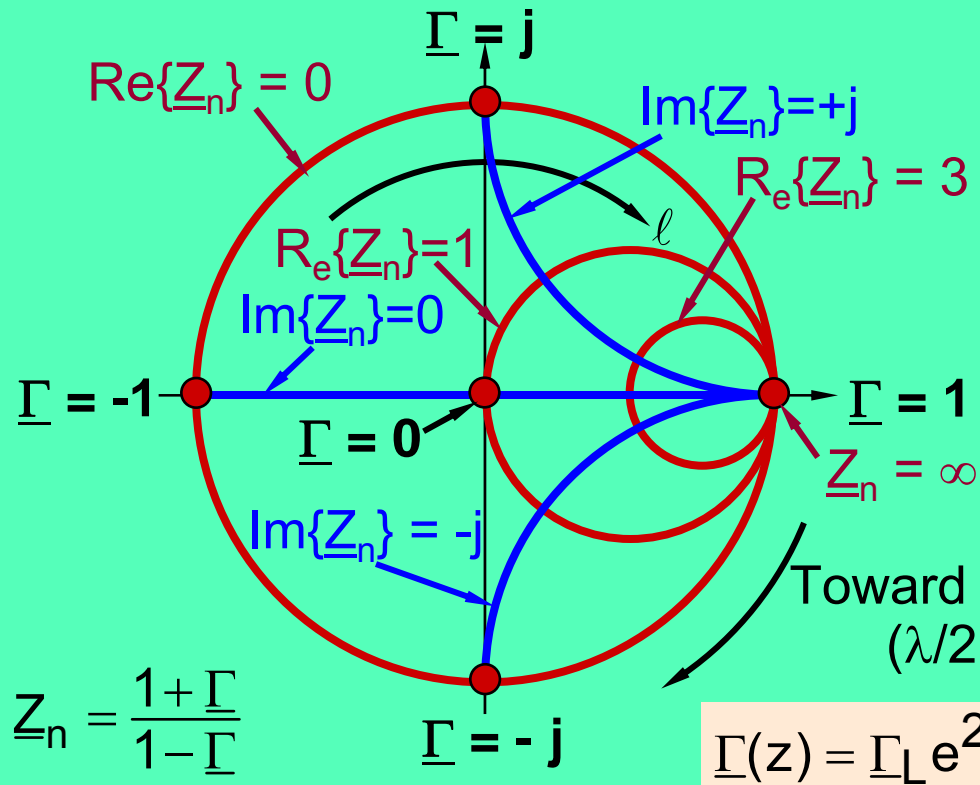
( $e^{j\phi} = \cos \phi + j \sin \phi$ )





# GAMMA PLANE $\Rightarrow$ SMITH CHART

## Gamma Plane:



$$\Gamma(z) = \Gamma_L e^{2jkz} = \Gamma_L e^{-2jkl}$$

Toward generator (larger  $l$ )  
 $(\lambda/2 \Rightarrow \text{full rotation})$

## Smith Chart = Gamma Plane + $Z_n(z)$ :

$$\frac{[Z_n(z) - 1]}{[Z_n(z) + 1]} = \Gamma(z) \quad \quad Z_n(z) \triangleq \frac{Z(z)}{Z_0} = \frac{[1 + \Gamma(z)]}{[1 - \Gamma(z)]}$$

$$Z_L \Leftrightarrow Z_{Ln} \Leftrightarrow \Gamma_L \Leftrightarrow \Gamma(z) \Leftrightarrow Z_n(z) \Leftrightarrow Z(z)$$